REMARKS

The proposed Amendments to the Specification have been provided to ensure correspondence between the Specification and the Formal Drawings filed herewith.

The Commissioner is hereby authorized to charge any fee deficiencies or credit any overpayments to Deposit Account 16-1340.

Respectfully submitted,

Dated: July 16, 2004

Thomas J. Perkowski, Esq.

Reg. No. 33,134

Attorney for Applicants

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1266 East Main Street

Stamford, Connecticut 06902

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CERTIFICATE OF EXPRESS MAILING UNDER 37 C.F.R. 1.10

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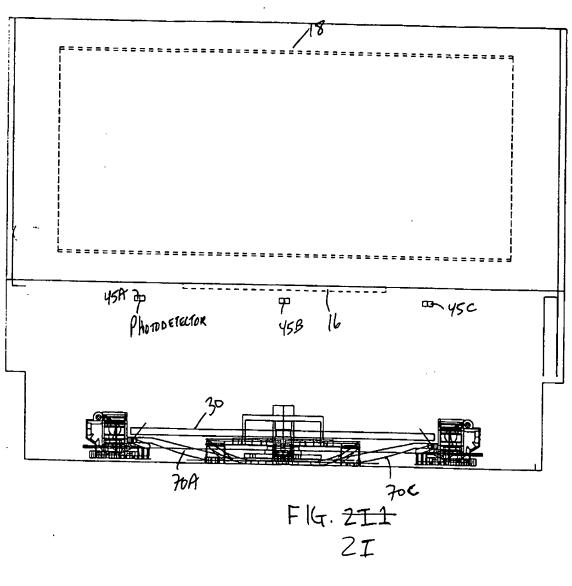
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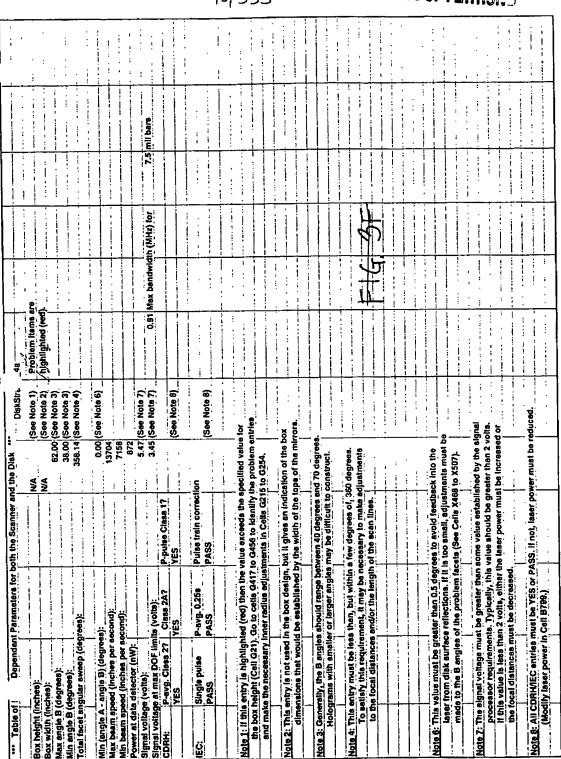


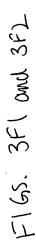


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d = distance	d = distance from disk to base of scanner (inches);	e of scanner (Inch.	100									
HOTEGORE! 81	Kotstones speed of disk (rpm)					5200						Maximum
												Collection
DiskStretos 4xia	4.116					SEO AM	6			1		Congenous
							1			٠l	Light	Area
	7.7				i	rocal plane	358.14		_	dead time for	Collection	(lgnoring
ĺ	-	Geometrical			Angle of	ecan line		Scan mult.	Rotation	1	Factor	notch)
7800	Focal length	Focal length	Angle A	Angle 8	Diffraction	length	Scan Angle	Factor (m)	Angle	1.15	1	,
	(Inches)	(inches)	(degrees)	(degrees)	(degrees)		(decrees)	1	(decrees)	(decrees)		1 1 20
	Given		Given	Given					-	Tool Road		(ad- 111.)
1	12.5	12.73							26.24	37.30	,	
2									20.00	66.33	00'1	
			:	:				:	28.35	29.50	0.60	
	12.7					:	İ		28.86	27.81	0.82	
•	1.3					į			29.19	30,34	0.71	!
	127	12.94					42.00		27.97	21.00	0.70	
•	12.0	12.21	52			İ		ľ	30.28	31 42	0.64	
7		15.08							27.99	20 14	10.0	
8	14.7	15.08	3 52		32.00	9.750		ľ	27.88	20.14	200	
8	13.5	13.80		60.00	30.00	9.750	39.71	30	30.65	31.8	22.0	10.1
2	13.5	13.60				9.750	39.71		30.65	31.80	22.0	2
=	14.8	15.19	3 52	62.00		9.750	38.48		8	30.34	60 0	00.
12	14.8	15.19	52	62.00		9.750	38.46	1.25	20 10	20.00	200	8.8
										5	3	

F14.341 F165 341A and 341B



TG (1227/39) TG (Notch size in mimo	ilmor					-			_			-	:
3.5 mm x 5.1 m (3.5 mm x 6.5 mm at disk) Design	TG (12/21/99)									T				•
Collection Col	3.5 mm x 5.1 m	14 (3.5 mm x 6.5 m	nm at disk)						NOTE: If any	entry in these	two columns is les	s than 0.5 degr	892	1
Area Beam speed Beam speed <td>Design</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>(Pigh</td> <td>lighted in red), t</td> <td>he corresponding</td> <td>B angle should</td> <td>be changed.</td> <td></td>	Design								(Pigh	lighted in red), t	he corresponding	B angle should	be changed.	
Area Beam speed Beam speed <td>Collection</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>This</td> <td>s accomplished</td> <td>t by modifying the</td> <td>"Distance from</td> <td>rotational axis</td> <td></td>	Collection								This	s accomplished	t by modifying the	"Distance from	rotational axis	
(Includes at max depth at min depth <td>Area</td> <td></td> <td></td> <td>Beam speed</td> <td></td> <td></td> <td></td> <td></td> <td>entry</td> <td>for that line (ce</td> <td>ile G46 to G85).</td> <td></td> <td></td> <td></td>	Area			Beam speed					entry	for that line (ce	ile G46 to G85).			
rolch lose of field of field engle function 0,035 lumber of faces function 0,035 lumber of faces function 1 faces function 0,035 lumber of faces faces<	(Includes		at max depth	at min depth	skew	Facet count								
eq. inches) (inches/sec) (inches/sec) </td <td>notch loss of</td> <td>scan line</td> <td>of field</td> <td>of field</td> <td>angle</td> <td>function</td> <td>Number of</td> <td></td> <td></td> <td>Ang</td> <td>le A - Angle B</td> <td></td> <td></td> <td></td>	notch loss of	scan line	of field	of field	angle	function	Number of			Ang	le A - Angle B			
sq. Inches/sec) (Inches/sec) (Inches/se	0.035	2				1 = facet	facets			(AD	solute value)	:	-	
2.27 11052 13704 8400 0 1 0.914 0.560 0.354 2.08 1.015 1.278 7502 0 1 0.851 0.550 0.353 2.08 1.095 1.278 7502 0 1 0.850 0.353 1.08 1.085 1.242 7286 0 1 0.856 0.343 1.78 1.0383 1.223 7830 0 1 0.856 0.343 1.37 1.47 9544 1/823 7830 0 1 0.856 0.343 1.37 1.47 9544 1/823 2.8 1 0.795 0.477 0.318 1.97 1.0492 1.634 8351 2.8 1 0.842 0.527 0.286 1.62 9524 11640 7407 2.8 1 0.776 0.494 0.282 1.62 9524 1.1068 1.206 0.535 0.272 0.282 </td <td>sq. Inches)</td> <td></td> <td>(Inches/sec)</td> <td></td> <td>(degrees)</td> <td>0 =no facet</td> <td>12</td> <td></td> <td></td> <td>9</td> <td>egrees)</td> <td></td> <td>:</td> <td>:</td>	sq. Inches)		(Inches/sec)		(degrees)	0 =no facet	12			9	egrees)		:	:
2.77 11052 13704 8400 0 1 0.914 0.560 0.354 1.81 10150 12738 7502 0 1 0.853 0.353 2.08 10395 13468 6331 0 1 0.893 0.343 1.63 9854 12468 7286 0 1 0.895 0.343 1.67 9544 1929 7188 0 1 0.856 0.327 1.67 9544 1929 7188 0 1 0.842 0.377 1.67 9524 1929 7407 28 1 0.842 0.586 1.62 9524 1640 7407 28 1 0.776 0.494 0.286 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 28 1 0.635 0.772 1.88 10066 <td></td> <td></td> <td></td> <td></td> <td></td> <td>:</td> <td></td> <td></td> <td>3andwidth</td> <td></td> <td></td> <td>; ;</td> <td></td> <td></td>						:			3andwidth			; ;		
1.81 10150 12798 7502 0 1 0.853 0.560 0.353 2.08 1.0895 13466 6321 0 1 0.898 0.555 0.343 1.63 98.56 12429 7286 0 1 0.856 0.343 1.78 10383 12835 7886 0 1 0.856 0.327 1.87 10492 12834 7158 0 1 0.856 0.327 1.87 10492 12834 28 1 0.842 0.557 0.286 1.62 9524 11640 7407 28 1 0.494 0.286 1.62 9524 11640 7407 28 1 0.494 0.282 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 28 1 0.694 0.695 1.88 <td< td=""><td>2.27</td><td></td><td></td><td></td><td></td><td>:</td><td>0.914</td><td>0.560</td><td>0.354</td><td></td><td>14.00</td><td></td><td></td><td></td></td<>	2.27					:	0.914	0.560	0.354		14.00			
2.08 10895 13468 8321 0 1 0.898 0.555 0.343 1 1.63 9856 12429 7286 0 1 0.829 0.486 0.343 1 1.79 10383 12835 7786 0 1 0.856 0.457 0.327 0 1.87 10492 12834 8351 28 1 0.042 0.557 0.286 1.62 9524 11640 7407 28 1 0.042 0.557 0.286 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 12108 8027 28 1 0.807 0.535 0.272 1.84 10068 12108 8027 28 1 0.807 0.872 0.272	1.81				0	-	0.853	0.500	0.353		12.00			
1,63 98.5e 12429 7286 0 1 0.829 0.486 0.341 1,79 10383 12835 7930 0 1 0.855 0.529 0.327 1,47 9544 11829 7715 0 1 0.795 0.477 0.316 1,57 10492 12634 8351 28 1 0.842 0.557 0.286 1,62 9524 11640 7407 28 1 0.776 0.494 0.282 1,62 9524 12108 8027 28 1 0.776 0.494 0.282 1,88 10068 12108 8027 28 1 0.807 0.535 0.272 1,84 1,0068 12108 8027 28 1 0.807 0.535 0.272	3 2.08				0	-	0.898	0.555	0.343		10.00			1
10383 12835 7750 7750 0 1 0.856 0.529 0.327 9544 11922 7750 7750 1 0.795 0.477 0.318 10492 12634 8351 -28 1 0.042 0.557 0.286 9524 11640 7407 28 1 0.776 0.494 0.282 9524 11640 7407 28 1 0.776 0.494 0.282 10068 12108 8027 28 1 0.807 0.535 0.272 10068 12108 8027 -28 1 0.807 0.535 0.272	1.83				0	1	0.829	0.486	0.343		8.00	1	-	
1.47 9544 11929 7158 0 1 0.795 0.477 0.318 1.57 10492 12634 8351 28 1 0.842 0.557 0.286 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.89 10068 12108 8027 28 1 0.807 0.535 0.572 1.89 10068 12108 8027 28 1 0.807 0.535 0.272	1.79				0	•	0.856	0.529	0.327		4.00			!
1.97 10492 12634 8351 28 1 0.842 0.557 0.286 1.97 10492 12634 8351 -28 1 0.842 0.557 0.286 1.62 9524 11640 7407 -28 1 0.776 0.494 0.282 1.63 10068 12108 9627 28 1 0.807 0.535 0.572 1.84 10068 12108 8027 -28 1 0.807 0.535 0.272	1.47				0	•	0.795	0.477	0.318		0.00			
1.97 10492 12834 8351 -28 1 0.842 0.557 0.286 1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 -28 1 0.776 0.494 0.282 1.88 10068 12108 8027 28 1 0.807 0.535 0.272 1 1.84 10068 12108 8027 -28 1 0.807 0.535 0.272 1	1.97				28	_	0.842	0.557	0.286		6.00			!
1.62 9524 11640 7407 28 1 0.776 0.494 0.282 1.62 9524 11640 7407 -28 1 0.776 0.494 0.282 1.88 10068 12108 8027 28 1 0.807 0.535 0.272 1.84 1.066 12108 8027 -28 1 0.807 0.535 0.272	76.1						0.842	0.557	0.286		00.9			
1.62 9624 11640 7407 -28 1 0.776 0.494 0.282 1.88 10068 12108 8027 28 1 0.807 0.535 0.272 1 1.84 10068 12108 8027 -28 1 0.807 0.535 0.272 1	1.62					_	0.776	0.494	0.282		8.00			
1.88 10068 12108 8027 28 1 0.807 0.535 0.272 1.88 10068 12108 8027 -28 1 0.807 0.535 0.272	1.62				-28	-	0.776	0.494	0.282		8.00		:	:
1.86 10069 12108 8027 -28 1 0.807 0.535 0.272					28	-	0.807	0.535	0.272		10.00			:
	1.88	10069	12108	8027	-28	-	0.807	0.535	0.272		10.00			

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F1G.3H F1GS. 3H1 Hrrough 3H3

A 10 10 10 10 10 10 10 10 10 10 10 10 10	Francisco Apple	to Corner for Box		Aldrini Getatin Swell ***										
DATE	Cuposone August	MODULA CADOSCIA PARTIES TO COLOR TO THE PARTIES OF				650	E							
DiskStratos 4.xls	4.ris			-										
Percent pela	tin swell (from m	Percent celetin awell (from measurements) dette-th:	:S:	Š	1			1	-					
				-			:		1		-			
	Exposure engine at 486 run	e at 488 mm	1	Bue ente	Exposure angles to compens	sate for awe!!	•						- University	Dete-0
	Reference	Object	Res	rence	Object	:	(we)ouwed	Jemme(sw)_[gamme(0)(A.	-					:
Facet	Been	Bean	Beam	E	Beem,		-							-
	(degrees)	(degrees)	(Gep)	(800)	degrees)		-		-					
					-						-			į
	26.00	20 00		23.85	40.50		8			:			:	:
-	2				20.70		13.6.		ı				1	:
	25.45		i: +: +: +: -: -: ::		2.00		8	!	:	į				
•	25.25	35.82		24.63	DQ.05		20.3	ļ	i		:			i
	28.12	8.8		25.35	35.04		-2.41	:			:	:	!	
	28.81	30.90	_	26.4	31,31		2.	•			;	;		
	27.6	27.53		27.53	27.53		000		:		:		:	
	20.00			28.28	21.77		1.92	!	;	:	!	:		
	28.64			29.28	21.77	!	1.92							-
	2002			28.83	19.60		2.58	•						-
9	29.02			29.89	19.83		2.58	3.10	6	9	600	200	10.01	11.58
=	29.40			8.50	17.89	-	3.25					!	!	
	47.00	00 00		95.05	17.89		325							

F14.3I F165. 3I | and 3I2

OiskStr. ,a



Anatyels	*** Analysis of the Focus Shift and Out-of-focus Spot Si	and Out-of-focu	5 Spot Size for Con	ize for Converging Reference Beam ***	nce Beam ***							
(Not applicab	Not applicable for Stratos)											
Convergenc	Convergence of the reference beam:	Yeam:		-1477 mm	. EE							:
Focal length	Focal length of parabolic mirror.	Ľ		58.83	EE						ŀ	
Distance fro	Distance from parabolic mirror to detactor:	to detector:		9	60 mm							
	Design	Par. Mirror		Object Image	Image		Spot size					
Facet	ngth	Eff. width	ngth	distance	distance	shift	at detector					
	(mm)	(mm)		(mm)	(EE)	(mm)	(mm)					
								0.88				
	317.50	4	40 404.42	-14858.75	59.05	-0.95	0.64	Distance (Cell I	5621) may ha	Distance (Cell E621) may have to be adjusted	Z	
	292.10	4	40 364.09	31841.43	58.71	-1.29	0.88	so that the max	dmum spot s	so that the maximum spot size at the detector in	or is	
₹7	322.58	4	40 412.69				09.0	approximately	the same whe	approximately the same when the 1/2 depth of fleid value	of fleld value	
4	292.10	4	40 364.09		58.71	-1.29	0.88	ls negative as i	I is when the	1/2 depth of fter	is negative as it is when the 1/2 depth of field value is positive.	.e.
•0	322.58	4	40 412.69		59.11		09'0	(The 1/2 depth	of field value	(The 1/2 depth of field value is located at Cell G19)	HG19)	
8	304.80	4	40 384.03	48230.76	58.89		0.75		Ι			
7	373.38	4	0 499.67	-4485.04	29.60	-0.40	0.27					
8		4	40 499.67	-4485.04	9.60		0.27					
8	342.90	4	40 446.55	-6818.26	59.33		0.45					
10	342.90	4	0 446.55	-6818.26	59.33	-0.67	0.45					
-	375.92	4	40 504.23	4375.15	59.62	-0.38	0.25					
12	375.92	4	40 504.23	4375.15	59.62	-0.38	0.25					

F19.33 F19.351 and 352

L .alos_4

The number of overlapping lines (N-overlap) must be determined from the scenner data. A safe assumption for our scanners is to consider that two scan lines are overlapped (ONLY when the difference between their diffraction angles (9) is less than 2 degrees.	· CDRH/IE	C Calculations to	Verify that the Sca	nner Mediskilierus	* CDRH/IEC Calculations to Verify that the Scanner Meels Hier and Polass Requirements ***	nts ***	
umber of overlapping lines (N-overlap) must be determined from the difference between their diffraction angles (B) is less to being equal, the slowest scan lines (largest angle B) will be less than the difference between their diffraction angles (B) is less than the difference between their diffraction angles (B) is less than the difference of laser (deg.): 0.0015 rilp: 1 5200 rilp: 0.0015 0.0015 rilp: 0.0015 0.0012 rilp: 0.0017 0.0012 rilp: 0.0018 0.0012 rilp: 0.0018 0.0012 rilp: 0.0018 0.0012 rilp: 0.0012 ri							
### about the difference between their diffraction angles (B) is less than the difference between their diffraction angles (B) is less than the difference between their diffraction angles (B) is less than the slowest scan lines (largest angle B) will be less than the slowest scan lines (largest angle B) will be less than than than than than than than than	The number	of overlapping lin	es (N-overlap) mus	st be determined fr	om the scanner date		
Seconds Seco	A safe assur	nption for our sca	nners is to consid	er that two scan iln	es are overlapped		
Pedrog equal, the slowest scan lines (largest angle B) will be riab: Speed (rpm):	ONLY when	the difference bet	ween their diffracti	on angles (B) is le	ss than 2 degrees.		
Page (rpm): 1 0.0015 0.0	All else bein	g equal, the slowe	st scan lines (larg	est angle B) will be	the worst case scal	lines.	
Seconds 1 1 1 1 1 1 1 1 1							
Speed (fpm):	N-overlap:						
Activergence of laser (deg.): 8 Activergence of laser (deg.): 30 Activergence of diffraction at MF plate (deg.): 30 Activergence of deg. (deconds): 30 Activergence of deg	Motor speed	(rpm):		5200			
S-divergence of laser (deg.): 30	Alpha-min (r	adlans):		0.0015	(from standard)		
Scalivergence of laser (deg.): 61	FWHM P-div	ergence of laser (c	leg.):	8	(Linked from Trnc	spreadsheet)	
Internation at MF plate (deg.): 29.23 29.2	FWHM S-div	ergence of laser (c	leg.):	30	(Linked from Trnc	spreadsheet)	
of Incidence at MF plate (deg.): 29.23 of diffraction at MF plate (deg.): 0.87 im): 3.93 ge source dimension (mm): 2.40 tree to aperture (mm	Focal length	of collimating len	9 (mm):	6.1	(Linked from Trnc	spreadsheet)	
of diffraction at MF plate (deg.): 42.12 imi): 3.93 ge source dimension (mm): 2.40 ire to aperture (mm): 2.40 (radians): 2.40 et window 7 mm transit 7 mm transit 7 mm transit 4 me at 4.0801E-05 3.9556E-05 3.9556E-05 4.0801E-05 4.0801E-05 4.0801E-05 6 6.0.86 4.0801E-05 4.0801E-05 6 6.0.87 4.00358E-05 6.0.87 4.00358E-05 6 6.	Angle of Incl	dence at MF plate	(deg.):	29.23			
10 10 10 10 10 10 10 10	Angle of diff	raction at MF plate	(deg.):	42.12			
ge source dimension (mm): 3.93 ge source dimension (mm): 2.40 tce to aperture (mm): 2.40 (radians): 2.00 Laser power tc (200) ti (actual) at window 7 mm transit 7 mm transit (mW) time at tim	Х-р (тт):			0.87			
ge source dimension (mm): (radians): (radians): Laser power tc (200) ti (actual) et window 7 mm transit 7 mm transit time at (mW) d = 200 mm actual d (seconds) 1 0.86 3.95856E-05 3.95856E-05 3.958356E-05 3.95	X-9 (mm):			3.93			
(radians): 200 (radians): 0.012 Laser power tc (200) ti (actual) at window 7 mm transit 7 mm transit (mW) time at time a	Average sou	rce dimension (mr	Ë	2.40			
(radians): 0.012 Laser power tc (200) tt (actual) P x tl et window 7 mm transit 7 mm transit 7 mm transit (mW) 4 me at clust of ime at dime	Distance to a	sperture (mm):		200	(actual distance or	200 mm, whichever is	greater)
Laser power tc (200) tt (actual) P x tf	Alpha (radia:	ns):		0.012			
Laser power tc (200) tt (actual) P x tl 4t window 7 mm transit 7 mm transit 7 mm transit 7 mm transit 4 = 200 mm actual d 6 = 200 mm actual d Facet count 2 0.86 3.95856E-05 3.95856E-05 0.0000339 Facet count 2 0.86 3.96549E-05 3.96549E-05 0.0000341 Facet count 2 0.86 4.08001E-05 3.96549E-05 0.0000341 Facet count 3 0.86 4.08011E-05 4.08015E-05 0.0000351 C0000370 4 0.86 4.20115E-05 4.08015E-05 0.0000352 C0000370 5 0.86 4.40086E-05 4.40086E-05 0.0000425 C0000430 6 0.87 4.90358E-05 4.90368E-05 0.0000430 C0000430 10 0.87 4.96126E-05 4.96126E-05 0.0000430 C0000430 11 0.87 5.14525E-05 0.0000446 0.0000446 0.0000446	Ge:			7.996			
Laser power tc (200) tt (actual) P x tl et window 7 mm transit 7 mm transit 7 mm transit 7 mm transit (mW) time at time at time at (Joules) (Joules) (Joules) Facet count 1 0 86 3.95856E-05 3.95856E-05 0.0000339 Facet count 2 0.86 3.96549E-05 3.96549E-05 0.0000341 Facet count 3 0.86 4.08001E-05 3.96549E-05 0.0000341 Facet count 4 0.86 4.0801E-05 3.96549E-05 0.0000351 Facet count 5 0.86 4.0801E-05 4.0815E-05 0.0000352 CO000370 6 0.87 4.40086E-05 4.40086E-05 0.0000425 CO0000425 7 0.87 4.90358E-05 4.90358E-05 0.0000430 CO000430 9 0.87 4.96126E-05 0.0000430 CO000430 CO000430 10 0.87 4.96126E-05 0.0000446 0.0000446 CO000446 11							
Laser power tc (200) tt (actual) P x tl et window 7 mm transit 8 x tl 9 x							
et window 7 mm transit 9 x ti 9 x ti (mW) time at				ti (actual)			
(mW) time at time at time at (Joules) d = 200 mm actual d Facends) 1 (seconds) (seconds) Facet count 2 0.86 3.95856E-05 3.95856E-05 0.0000341 Facet count 2 0.86 3.96849E-05 3.96549E-05 0.0000341 Facet count 3 0.86 4.0801E-05 3.96549E-05 0.0000341 Facet count 4 0.86 4.0801E-05 4.0800352 Count Count 5 0.86 4.08315E-05 4.0800352 Count Count 6 0.87 4.40016E-05 4.4000352 Count Count 7 0.87 4.90358E-05 4.40066E-05 4.90358E-05 0.0000425 Count 9 0.87 4.96126E-05 4.96126E-05 0.0000430 Count Count 11 0.87 5.14525E-05 0.0000446 Count Count Count 12 0.87 5.14525E-05 0.0000446<				7 mm transit	Pxt		
d = 200 mm actual d Facet count (seconds) (seconds) Facet count 0.86 3.95856E-05 3.95856E-05 0.0000339 Facet count 0.86 3.96549E-05 0.0000341 Facet count 0.86 4.0801E-05 0.0000341 Facet count 0.86 4.0801E-05 0.0000352 Facet count 0.86 4.28116E-05 4.080316E-05 0.0000370 Facet count 0.87 4.40086E-05 4.40086E-05 0.0000430 Facet count 0.87 4.96126E-05 4.90358E-05 0.0000430 Facet count 0.87 4.96126E-05 4.96126E-05 0.0000430 Facet count 0.87 5.14525E-05 0.0000446 Facet count	Facet	(mM)	time at	time at	(Sonles)		
(seconds) (seconds) (seconds) Facet count 0.86 3.95856E-05 3.95856E-05 0.0000339 Facet count 0.86 3.96549E-05 3.95856E-05 0.0000341 Facet count 0.86 4.08016E-05 0.0000351 COUNT COUNT 0.86 4.28115E-05 0.0000370 COUNT COUNT 0.87 4.40086E-05 4.40086E-05 0.0000430 COUNT 0.87 4.90126E-05 4.90358E-05 0.0000430 COUNT 0.87 4.96126E-05 4.96126E-05 0.0000430 COUNT 0.87 5.14525E-05 0.0000446 COUNT COUNT			d = 200 mm	actual d			
0.86 3.95856E-05 3.95856E-05 0.0000339 0.86 3.96549E-05 3.95856E-05 0.0000341 0.86 4.08001E-05 0.0000351 0.86 4.08156E-05 4.08001E-05 0.0000370 0.86 4.28115E-05 0.0000370 0.87 4.40086E-05 4.40086E-05 0.0000430 0.87 4.96126E-05 4.96126E-05 4.96126E-05 0.87 5.1452E-05 5.1452E-05 0.0000446 0.87 5.1452E-05 5.1452E-05 0.0000446			(seconds)	(seconds)		Facet coun	
0.86 3.95856E-05 3.95856E-05 0.0000339 0.86 3.96549E-05 3.96549E-05 0.0000341 0.86 4.08001E-05 4.08001E-05 0.0000351 0.86 4.08115E-05 4.08011E-05 0.0000352 0.87 4.40086E-05 4.40086E-05 0.0000425 0.87 4.90538E-05 4.90358E-05 0.0000430 0.87 4.96126E-05 4.96126E-05 0.0000430 0.87 5.14528E-05 5.14528E-05 0.0000446 0.87 5.14528E-05 5.14528E-05 0.0000446							
0.86 3.96549E-05 3.96549E-05 0.0000341 0.86 4.08001E-05 4.08001E-05 0.0000351 0.86 4.0815E-05 4.08015E-05 0.0000352 0.86 4.28115E-05 4.08315E-05 0.0000370 0.87 4.40086E-05 4.40086E-05 0.0000425 0.87 4.90358E-05 4.90358E-05 0.0000430 0.87 4.96126E-05 4.96126E-05 0.0000430 0.87 5.14525E-05 5.14525E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446	_	98'0	3.95856E-05	3.95856E-05	0.0000339		-
0.86 4.08001E-05 4.08001E-05 0.0000351 0.86 4.08315E-05 4.08315E-05 0.0000352 0.86 4.28115E-05 4.08315E-05 0.0000370 0.87 4.40086E-05 4.40086E-05 0.0000425 0.87 4.90358E-05 4.90358E-05 0.0000430 0.87 4.96126E-05 4.46126E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446	2		3.96549E-05	3.96549E-05	0.0000341		1
0.86 4.08315E-05 4.08315E-05 0.0000352 0.86 4.28115E-05 4.28115E-05 0.0000370 0.87 4.40086E-05 4.40086E-05 0.0000425 0.87 4.90358E-05 4.90358E-05 0.0000425 0.87 4.96126E-05 4.96126E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446	9		4.08001E-05	4.08001E-05	0.0000351		1
0.86 4.28115E-05 4.28115E-05 0.0000370 0.87 4.40086E-05 4.40086E-05 0.0000381 0.87 4.90358E-05 4.90358E-05 0.0000425 0.87 4.96126E-05 4.90368E-05 0.0000430 0.87 4.96126E-05 4.96126E-05 0.0000430 0.87 5.14525E-05 5.14525E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446	4		4.08315E-05	4.08315E-05	0.0000352		1
0.87 4.40086E-05 4.40086E-05 0.0000381 0.87 4.90358E-05 4.90358E-05 0.0000425 0.87 4.90358E-05 4.90358E-05 0.0000430 0.87 4.96126E-05 4.96126E-05 0.0000430 0.87 4.96126E-05 5.14525E-05 0.0000446 0.87 5.14525E-05 5.14525E-05 0.0000446	5		4.28115E-05	4.28115E-05	0.0000370		1
0.87 4.90358E-05 4.90358E-05 0.87 4.90358E-05 4.90358E-05 0.87 4.96126E-05 4.96126E-05 0.87 4.96126E-05 4.96126E-05 0.87 5.14525E-05 5.14525E-05 0.87 5.14525E-05 5.14525E-05	9		4.40086E-05	4.40086E-05	0.0000381		-1
0.87 4.90358E-05 4.90358E-05 0.87 4.96126E-05 4.96126E-05 0.87 4.96126E-05 4.96126E-05 0.87 5.14525E-05 5.14525E-05 0.87 5.14525E-05 5.14525E-05	7		4,90358E-05	4.90358E-05	0.0000425		1
0.87 4.96126E-05 4.96126E-05 0.87 4.96126E-05 4.96126E-05 0.87 5.14525E-05 5.14525E-05 0.87 5.14525E-05 5.14525E-05	8		4.90358E-05	4.90358E-05	0.0000425		1
0.87 4.96126E-05 4.96126E-05 0.87 5.14525E-05 5.14525E-05 0.87 5.14525E-05 5.14525E-05	6		4.96126E-05		0.0000430		1
0.87 5.14525E-05 5.14525E-05 0.87 5.14525E-05 5.14525E-05	10		4.96126E-05		0.0000430		-
0.87 5.14525E-05 5.14525E-05	11		5.14525E-05		0.0000446		1
	12		5.14525E-05	5.14525E-05	0.0000446		



F14.312 F165.3124 and 3128

Duty Cycle:	0.0044502+2	::	! ;			word to see the control of the contr	
	_:						
Paverage Is	the sum of the ove	erlap Pi x tł produc	Paverage is the sum of the overlap PI x it products divided by the sum of the ti times times the duty cycle	um of the ti th	mes times the d	uty cycle	
Paverage is,	, therefore, the sur	n of the overlap PJ	Paverage is, therefore, the sum of the overlap PI x it products times the rps of the motor.	the rps of the	e motor.		
CDRH Calcu	CDRH celculations and results		:	:		:	
:			Class 1	Class 27	Class 2A?	: : : : : : : : : : : : : : : : : : : :	
Pavg. (mW):	:	0.003869		YES	YES		
				:	· }		-
P (single pulse) (mW): (Maximum allowed)	lse) (mW): llowed)	8.27	. :				
				:		:	-:
P (single pulse) (Actual)	(98)	0.87 YES	VES	! : ! :	: :	: :	: ; : :
JEC nelculati			: .	1			: .
			:	:		:	
IEC condition	EC condition A (Single pulse)		· .	: :	PASS/FAIL		
P (eingle puise) (mW):	se) (mw):	70.6		:	PASS		
(Maximum allowed)	(pewol)	:	!!!	. !		:	į
:	ě e			:	,		
IEC condition	B (average power	IEC condition B (average power in a 0.25 second pulse train)	oulse train)		:		
Pavg. allowed (mW):	d (mW):	7.92			PASSIFAIL	:	:
Pava, scenner (mW):	l sr (mW):	95000					
					2		
IEC condition	EC condition C (pulse train correction factor)	rection factor)	!				
(For this cate. —	utation, you need t	o insert the sum of	(For this calculation, you need to insert the sum of the pulse times in the overlapping scan lines)	the overlapp!	ing ecan lines)	: :	1
		:			!		
(sum of pulse times	ids):	0.000051					
III OVATIAL BCATI IIII 08)	an Imes)	-	-	:	:		
Pmax (mW):		1.99	•				
Number of pulses in train;	lses in train;	21.67	1 :				
Correction factor	ctor:	0.4635	: :				:
Pmax (PT corrected)(mW):	rected)(mW):	30.63			PASS/FAIL		
Pw (including overlap)	overlap)	0.87			PASS		
		-		: :			



×					Z	0.562	-0.923	0.801			ers	7												he abor			Γ				
Μ				End	^	-0.367	-0.367	0.098			Mirror 3 Comers	>												The second part of mirror 2 is the abo			ĺ				<u> </u>
^					×	0.741	-0.117	-0.590			Mirro	×												art of mir	Ī						
n			Γ		Γ				Γ					Г			Г	Г	Γ	Γ	Г		T.	ğ	r	T	T	Г	T		
⊢					7	0.616	-0.990	0.667			ers	7	-0.112	0.382	1.066	1.066	0.175							he secor		-0.112	0.382	1.066	1,066	0.175	
S				Middle	^	0.000	000	0.448			Mirror 2 Comers	^	0.000	0.000	-2.256	-2.256	1.000							_	1	0.000	0.000	2.256	2.256	1.000	
æ					×	0.788	-0.140	-0.595			Mirro	×	3.000	4.800	5.071	5.071	3.060					!		for mirre	<u> </u>	3.000	4.800	5.071	5.071	3.060	
σ	Γ								Г				_						┢		_			lirror			T	H	Т	-	
٥		Z	0.788		2	0.616	-0.990	0.667	_		ers	Z	2.509	1.728	1.728	2.509								a split m							
0	-	λ	0.000	End	λ	0.000	0.000	0.448			Mirror 1 Comers	λ	-1,600	-2.400	2.400	1.600	•							station uses a split mirror for mirror #2.							
z	Facel	×	-0.616		×	0.788	-0.140	-0.595			Mirro	×	3.750	5.100	5,100	3.750								This stati							
	46	47	48	49	20	51	25	53	22	55	56	27	28	29	8	61	82	છ	ል	65	99	29	69	69	20	71	72	73	74	75	16

FIG. 6D2



			Γ			<u>8</u>	6	87		Γ	Г			Γ	Γ	Г	Γ			Γ	Τ			Ŕ	Τ	Γ	Ė	Γ	Г	Ι-,	Г
٧					2	0.581	-0.907	0.787			Sers	7												the at							
١٧				End	λ	-0.395	-0.395	0.062			Mirror 3 Comers	λ												ror 2 is							
AH					×	0.711	-0.149	-0.614			Mirr	×												The second part of mirror 2 is the abo							
AG																								ם	ſ						T
AF					Z	0.643	-0.985	0.647			ers	7	-0.112	0.382	1.066	1,066	0.175							he seco		-0.112	0.382	1.066	1.066	0.175	
AE				Middle	У	0.000	0.000	0.440			Mirror 2 Corners	λ	0.000	0.000	-2.256	-2.256	-1.000								<u> </u>	0.000	0.000	2.256	2.256	1.000	
PΩ					×	0.766	-0.175	-0.623			Mirro	×	3.000	4.800	5.071	5.071	3.060							for mirre		3.000	4.800	5.071	5.071	3.060	
AC									Г													T		nirror	┢		┢				-
AB		2	0.788		2	0.643	-0.985	0.647			ers	Z	2.509	1.728	1.728	2.509								a split n			-				
AA	2	λ	0.000	End	λ	0.000	0.000	0.440			Mirror 1 Comers	λ,	-1.600	-2.400	2.400	1.600	-							sesn uo							
7	Facet	×	-0.616		×	0.766	-0.175	-0.623			Mirro	×	3.750	5.100	5.100	3.750						_		This station uses a spllt mirror for mirror #2.						_	
	46	47	48	49	20	51	25	53	2	22	26	22	88	29	8	61	62	ន	8	65	99	29	89	69	2	71	72	73	74	75	9/

F14. 603

Station 2



	Φ	ď		2	ū	-	G		Ŀ	-		[-
4	Low Flevetion	Facet	7	,	1	-	,		1	,	2	7
4		×) >	7	T	Ī						
48	48 Vector from Module	-0.616	0.000	0.788	T							
49			End	i	Γ		Middle				E	
ය		×	^	2	Г	×	^	z		×	^	2
51		0.743	0.000	0.669		0.743	0.000	0.669		0.697	-0.362	0.619
25	First Mirror Reflected Directions	-0.209	0.000	-0.978		-0.209	0.000	-0.978		-0.189	-0.362	-0.913
23	Second Mirror Reflected Directions	-0.649	0.433	0.625	-	-0.649	0.433	0.625		0.648	0.089	0.757
ጷ	Third Mirror Reflected Directions				r						į	
જ												
26		Mirro	Mirror 1 Corners	ers	Г	Mirro	Mirror 2 Corners	lers.		Mir	Mirror 3 Comers	ers
22		×	_	2		×	^	2		×	>	7
28		3.750	-1.600	2.509	Г	3.000	0.000	-0.112	Γ			
59	2	5.100	-2.400	1.728		4.800	0.000	0.382				
8	8	5.100	2.400	1.728		5.071	-2.256	1.066				
6	4	3.750	1.600	2.509		5.071	-2.256	1.066				
62	9				Г	3.060	1.000	0.175				
83	9			-	<u> </u>]		
8	4				<u> </u>							
65	8				\vdash				Γ			
8					T		:					Ī
29			-		<u> </u>				Γ			
88								-	Ī			
69	Note: Special Case!	This station uses a split mirror for mirror #2.	ion uses	a split m	Ē	for mire		he seco	B	art of mi	The second part of mirror 2 is the abo	he abo
70			-		一							
_	Second Part of Mirror 2				H	3.000	0.00	-0.112				
2						4.800	0.000	0.382	Γ			
2					H	5.071	2.256	1.066				
7						5.071	2.256	1.066				
25					Н	3.060	1.000	0.175				
9					-							
					\dashv							
					ĺ				l			

F1G.604

Station 2



A Nimor 1 Corners A Nimor 1 Cor	3 -0.616 0.000 0.788 End End End Color 0.695 0.00 0.695 0.00 0.0243 0.000 0.037	8 -0.616 0.000 0.788 End End End Color 0.695 0.00 0.695 0.00 0.0243 0.000 0.037	8 -0.616 0.000 0.788 End End End Color 0.695 0.00 0.695 0.00 0.0270 0.00 0.0370 0.00 0.0370 0.00 0.0370 0.00 0.0	8 4	┝╌╣╩╽╌╏	AM Y	AN	AO	AP		Q	AQ AR	$\vdash\vdash$	AA	AR AS
X	X	Name	Name	8	9	Ш	0.788								
A y z y z y z y y z y y z y y z y y z y y z y y z y y z y y z y y z y y z y y z y y z y y z y y z z y z y z y z z y z z y z z y z z y z z y z z z y z z z z z y z	Mirror 1 Corners A y z y z y 0.0719 0.0719 0.0519 0.0519 0.0575 0.425 0.603 0.0519 0.	A	A Nicot Comers A Nicot Comers A Nicot Comers A Nicot Comers A Nicot Comers B 5.100 2.400 1.728 5.6 5.100 2.400 1.728 5.6 This station uses a split mirror for 5.00	<u>위</u>		ᇤ				≥	iddle	Middle	liddle	liddle	liddle End
0.719 0.000 0.695 0 -0.243 0.000 -0.970 -00.675 0.425 0.603 -0. Mirror 1 Corners	0.719 0.000 0.695 0 -0.243 0.000 -0.970 -0.0 -0.675 0.425 0.603 -0.0 Mirror 1 Comers x y z x x y z x x y z x x y z x x y z x x x y z x x x y z x x x y z x x x y z x x x y z x x x x	0.719 0.000 0.695 0. 2 -0.243 0.000 -0.970 -0.0. 3 -0.675 0.425 0.603 -0.0. Mirror 1 Corners	0.719 0.000 0.695 0. 2 -0.243 0.000 -0.970 -0.0. 3 -0.675 0.425 0.603 -0.0. Mirror 1 Corners	င္တ	-		7		×		^				Z
Mirror 1 Corners x x y 3.750 -2.400 1.728 4.4 5.100 2.400 1.728 5.6 3.750 1.600 2.509 5.6	Mirror 1 Comers x x y 3.750 -1.600 2.509 5.100 -2.400 1.728 5.100 2.400 1.728 5.100 2.400 1.728 5.100 2.400 1.728 5.100 2.400 1.728 5.100 2.400 1.728 5.100 2.509 5.100 2.509 5.100 2.509 5.100 2.509 5.100 2.509	Mirror 1 Corners x y z x 3.750 -2.400 1.728 5.100 2.400 1.728 5.1	Mirror 1 Corners	នាត	0.739	4	0.695	1	0.719	L	88	0.000 0.695	0.000 0.695	0.695	0.695 0.664
Mirror 1 Corners	Mirror 1 Comers	Mirror 1 Comers x y z 3.750 -1.600 2.509 3.0 3.750 1.600 2.400 1.728 5.100 2.400 1.728 5.100 3.750 1.600 2.509 3.0 3.100 This station uses a split mirror for 4.8	Mirror 1 Comers x y z 3.750 -1.600 2.509 3.00 3.750 1.600 2.509 3.750 1.600 2.509 3.00 This station uses a split mirror for 4.89	ાજ	-0.675		0.603	T	-0.675		25	_1_	_1_	0.603	0.603
Mirror 1 Corners	Mirror 1 Comers x y 2 3.750 -1.600 2.509 3.0 5.100 2.400 1.728 5.100 2.400 1.728 5.100 2.400 1.728 5.101 2.400 1.728 5.101 3.750 1.600 2.509 5.101 3.750 1.600 2.509 3.0	Mirror 1 Comers 2	Mirror 1 Comers 2	8		┖		Γ		1	1			2000	200.0
Mirror 1 Corners Mirror x x y z x x y z 2 x x y 2 2 x x y 2 2 x x y 2 2 x x x y 2 2 x x x y 2 2 x x x x	Mirror 1 Corners x y z y z 3.750 -1.600 2.509 3.6 5.100 2.400 1.728 5.6 3.750 1.600 2.509 5.6 3.750 1.600 2.509 3.0 This station uses a split mirror for 3.0	Mirror 1 Corners x y z y 3.750 1.600 2.509 3.00 3.750 1.600 2.509 3.750 1.600 2.509 3.100 3.100 This station uses a split mirror for the station uses a split mirror for	Mirror 1 Corners x x y z x y z x y z x y z x y z x y z x y z x y z x y z x y z x y z x y z y z y z x y z x y z x y z x y z x y z x y z x y z x y z x y z x y z x y x y x x y x y x x y x x x y x x x y x x x x y x x x x x x x x x x x x x	25				T							
3,750 -1,600 2,509 3,000 5,100 2,400 1,728 4,800 3,750 1,600 2,509 5,071 3,750 1,600 2,509 3,060	x y z x 3.750 -1,600 2,509 3,000 5,100 2,400 1,728 5,071 3,750 1,600 2,509 5,071 3,750 1,600 2,509 5,071 This station uses a split mirror for mirro	3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 4.800 3.750 1.600 2.509 5.071 3.750 1.600 2.509 3.060 This station uses a split mirror for mirro	3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.750 1.600 2.509 3.060 This station uses a split mirror for mirro	8	Mirr	or 1 Com	ers		Mir	or 2 C	Įģ	omers	omers		Somers Mirror 3 Comers
3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 4.800 5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071	3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 4.800 3.750 1.600 2.509 5.071 3.750 1.600 2.509 5.071 This station uses a split mirror for mirro	3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 4.800 3.750 1.600 2.509 5.071 3.750 1.600 2.509 5.071 This station uses a split mirror for mirro	3.750 -1.600 2.509 3.000 5.100 -2.400 1.728 4.800 3.750 1.600 2.509 5.071 3.750 1.600 2.509 5.071 This station uses a split mirror for mirro	57	×	λ	2		×	>		7	Z	*	*
5.100 -2.400 1.728 4.800 5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071	5.100 -2.400 1.728 4.800 5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.060 This station uses a split mirror for mirro	5.100 -2.400 1.728 4.800 5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.060 This station uses a split mirror for mirro	5.100 -2.400 1.728 4.800 5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.060 This station uses a split mirror for mirro	88	3.750	-	2.509		3.000	0	Ø	1 .	1 .	-0.112	-0.112
5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.060	5.100 2.400 1.728 5.071 3.750 1.600 2.509 5.071 3.060 This station uses a split mirror for mirro	3.750 1.600 2.509 5.071 3.060 2.509 5.071 2.000 2.509 5.071 2.000 2.509 5.071 2.000 2.509 5.071 2.000 2.000 2.509 2.000	3.750 1.600 2.509 5.071 3.060 1.71	က္က	9.100		1.728		4.800	0.0	Š		0.382		0.382
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3.060	3.060 This station uses a split mirror for mirror	3.060 This station uses a spilt mirror for mirror	3.060 This station uses a spift mirror for mirror	ᆵ	3.750		2.509		5.071	-2.2	ဖွ	36 1.066			
2	This station uses a split mirror for mirro	This station uses a split mirror for mirro	This station uses a split mirror for mirro	22					3.060	7.0	2	0.175	1	1	1
25 SS SS SS SS SS SS SS SS SS SS SS SS SS	This station uses a split mirror for mirro	This station uses a split mirror for mirro	This station uses a split mirror for mirro	й							1 ~				
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8	This station uses a split mirror for mirro	This station uses a split mirror for mirro	This station uses a split mirror for mirro 3.000 4.800	ø				\vdash			1				
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	3.000	3.000	3.000	$\overline{}$		-		\vdash	ŀ		1	1	1	1	
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	_	47	48	49	20	51	52	23	54	25	98	22	28	28	9	61	62	છ	8	65	99	29	88	69	2	71	72	73	74	75
¥	Facet	×	-0.616		×	699.0	-0.310	-0.724			Mirr	×	3.750	5.100	5.100	3.750								This stat						
AY	2	>	0.00	End	λ	000'0	0.000	0.407			Mirror 1 Comers	y	-1,600	-2.400	2.400	1.600								This station uses a split mirror for mirror #2.						
ΑZ		7	0.788		2	0.743	-0.951	0.557			ers	Z	2.509	1.728	1.728	2.509								a split n						
ВА																					Г			nirro				\vdash	Г	Г
88					×	699'0	-0.310	-0.724			Mirr	×	3.000	4.800	5.071	5.071	3.060							r for mire		3.000	4.800	5.071	5.071	3.060
ЭВ				Middle	λ	0.000	0.000	0.407			Mirror 2 Corners	`	0.000	0000	-2.256	-2.256	-1.000								1	0.000	0.000	2.256	2.256	1.000
80			i L		Z	0.743	-0.951	0.557			ners	7	Ľ.	0.382	1.066	1.066	0.175							The second part of mirror 2		-0.112	0.382	1.066	1.066	0.175
BE										ļ	!											Г		<u>g</u>	一			-	Г	
BF					×	0.634	-0.298	-0.730			Mirr	×												art of mir						
98				End	λ	-0.311	-0.311	0.114			Mirror 3 Comers	_												ror 2 is	Γ					
ᇤ					Z	0.708	-0.903	0.673			ners	Z												is the abo						

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WA	200	:																							xis. I.e.:			 			
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á			7		×	0.616	0.376	0770-			Mirro	×	3000	4.800					\dagger	T	\dagger			or mirro	-	3000	1	1	1	L	1
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4		2	•		Z	0.788	-0.927	0.508		T	ers	2	2.509	1.728	1.728	2.509				Ĺ	\dagger			s Split m	-		+	+	-	-	+
Í	9	λ	0.000	End	^	0.000	0.00	0.387			Mirror 1 Comers	>	-1.600	-2.400	2.400	1.600						-		n uses	-	\vdash	-		-	_	
	Facet	×	-0.616		×	0.616	-0.376	-0.770			Mirro	×	3.750		5.100	3.750	 		}- 			- - 		This station uses a split mirror for mirror #2	-		\vdash				L
	_	47	48	6	S	21	52	53	장	55	26	27	28	23	8	5	8	ន	ठ	65	99	29	88	69 TI	02	71	72	23	72	75	19/

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-Station 2



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F1G. 9 FlGs. QA Harough

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TWICEIRIOS-6-Politie
Degrees to reclare conversion lector:
1. 0.01143333
Truncation ensights, Effect of truncation on the diffraction Writted appl size of a Gaussian beam

Over the laser and lens parameters, this spreadahest will calculate the effect of truckation on the beam The light result is an "effective dismesser." This is an equitablent the equated demostratist will produce it he seems spot extra at he focal point as the scrial truckated beam. This is also the beam dismoser that will be inserted in the main scanner data design appreadant. The is also the beam The actual for more likibed to the main scanner data design appreadant. In the standard in the main appreadation will be a rounded number.

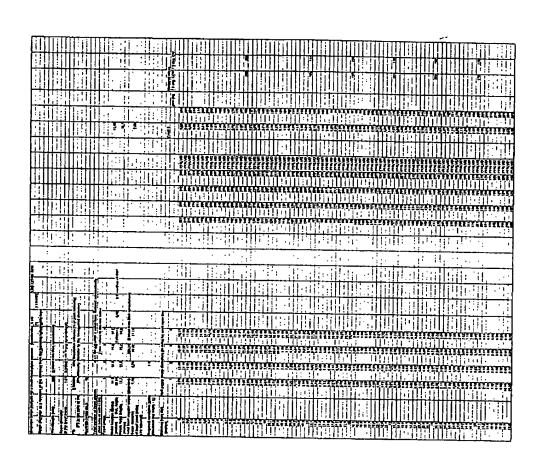
Subitativs	Wavelength (nm) Thera-P (degraes) Thera-S (degraes)	9 * 9 *			M = Moye; K = Kodeb; P = Philips; O = GelTech (Alternate choices - from Tom's teble)	Kodek; P Skee - Iro	- Philips; O m Tom's tebi	. Gelfech										
	focal length (mm) Numerical Aberture	0.130430 8 9.15		11 0.3	1 KAN 1 0 10 10 10 10 10	1	KV77 PIACOS2 PIAC325 PIAC320 WA128	P/AC325 8 8.1	P/AC320 7.5 0.3		7.00	WAG2 6.67 0.33	HVAN11 P/AC355 6.25 6.25 0.4 0.35		PVAS1 6 0.4	5.4 5.4 0.38	1.0 0.30 0.36 0.360 0.36	850330 G 6.1 0.16
Ne-squared be	Chear Aparture (rim) (e.2 at it NA) (h-squared beam diameter at lasts (rim)	02.1 881.1	1.50 fors down .188	4.6			2.0 2.0 3.0		22	32	3 =	3 %	3 4	22	ទិង	5 ° °	8,2	25
	Aperture factor (m)	1.263		m = 1 te 1/e-equerad truncetion m > 2 te essentially no truncation	dered thuncedo	و ۾												
28	Ne-squered beem radius (for normalized apenius)	0,792																
Truncation factor:	1,219		1/e-equere Incressed (Me-equared radius as local plane is 'n Increased by this lactor due to truncation.	il plene la " ue to truncation	نے												
(4274) (4274)	20; 3,078 (4/20/4(0)/~2 0.135353 Lr([4/20/4(0)]~2) - 2.00000001	80-	To determinely yeary ZO united aqual value of the Case of the SOLVE	To determine the effective dismeter, very ZO until (AZOyA(0))**2 = 0.1953353 ox, equivalently, until La((AZOyA(0))*2)**2. This can most seaty be done by white the SOLVER function of Exet Tools:	dismeter, 2 = 0.135335 o D/A(0)]*2]=-2 are by ueling reel Tools:	٠												
Effective diameter:	491: 0.97	_	Target	Target cell = \$C\$31; Value = -2 Change cell = \$C\$29	ilue = -2													
Spreadsheet value:	1.50		This is the is impact to and the ma	This is the effective beam diameter that is imked to the Caus spreadshes: and the main disk dealin spreadshest.	diameter that adsheet spreadsheet.													

The remetring part of this apreadables is simply the numerical integration to the distriction equals of the filt from the Matriced program. It heliutes the evaluation of the functions (A[ZyA(0)])²2 and Ln((A[ZyA(0)])²3), it also heliutes a graph of (A[ZyA(0)])²3 to Z.

5	A(Z) A(Z) elc.	0 16-0 16-0 16-0 16-0 16-0 16-0 16-0 16-
a 7-61460	(1Z)Y	0, \$494.1E.00 0,00198927 0,000198927 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921 0,000198921
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PIGS. 11A1A through 11A1H





士 F16 1181 P165. 11B1A through



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FIGS. 1182A through 1182E



≥			2.10576	2.21298	2.21298	2.46771	2.33696	2.05933	2.05933	1.94186	2.10576	2.01383	1.97666	1.93026	
_			1.75935	1.66502	1.66502	1.44090	-1.53897	-1.76326	-1.76326	1.85821	1.75935	0.83137	0,0000	-0.89961	
¥	Facet	4	4.82799	4.68407	4.68407	4.34215	4.17995	4.50146	4.50148	4.63750	4.82789	4.84129	4.79689	4.75856	
-			2.03365	2.14196	2.17507	2.49402	2.36336	2.00915	1.98718	1.86903	2.03365	1.94798	1,91369	1.86356	
-			1.81870	1.72980	1.86942	1,51260	-1.55897	-1.91413	-1.77513	-1.86391	1,81870	0.88565	00000	0.91710	
Ŧ	Facel	3	4.92433	4.77964	4.75362	4.31720	4.14486	4.54753	4.59009	4.72764	4.92433	4.92928	4.87537	4.83778	
5			1.96715	2.06571	2.06667	2.37191	2.24765	1.91239	1.91177	1.80291	1.96715	1.87935	1.85000	1.79393	
	-		1.88093	1.79109	1.79549	1.51422	-1.52325	-1.80322	-1.79883	-1.88882	1.88093	0.94389	0.00000	-0.94701	
æ	Facet	2	5.01400	4.88136	4.88064	4.46955	4.29296	4.68022	4.68147	4.80732	5.01400	5.02116	4.95474	4.92129	
			1,89155	1.98969	2.03847	2.31542	2.18575	1.86940	1.83693	1.72862	1.89155	1.80878	1.78542	1.72464	-
0			1.95380	1.86904	2.08109	1.69707	-1.63559	-2.01784	-1.80620	-1.89063	1.95380	1.00830	0.0000	-0.96140	
8	Facet	-	5.11617	4.98460	4.94695	4.55990	4.35785	4.71038	4.77395	4.89971	5.11617	5.11614	5.03523	5.00607	
A			Point 1	Point 2	Point 3	Point 4	Point 5	Point 6	Point 7	Point 8	Point 9	Start of scan fine	Middle of rotation	End of scan line	
	106	107 G3	108	601	110	111	112	113	114	115	116	117	118	119	120

FTG-1343 Fles. 13A3A and



2			0.09731	0.07610	0.07610	0.02898	0.08649	0.14032	0.14032	0.16470	0.09731	0.11760	0.13978	0.16575	
-			2.49916	2.46924	2.46924	2.40274	-1.79742	1.93323	-1.93323	-1.99474	2.49916	1.80404	0.29297	1.27076	T
¥	Facet	4	3.63985	3.48464	3.48464	3.13971	3.03925	3.40752	3.40752	3.57430	3.63985	3.70025	3.67474	3.66999	
ا ا			0.13136	0.10897	0.10205	0.04122	0.09718	0.16749	0.17186	0.19711	0.13136	0.15114	0.17070	0.19685	<u> </u>
-			2.57127	2.54596	2.66161	2.51989	1.84718	-2.08109	-1.96992	-2.02808	2.57127	1.82246	0.27090	1.26997	
Ŧ	Facet	6	3.89207	3.72893	3.69351	3.24144	3.10957	3.58373	3.62849	3.80192	3.89207	3.94222	3.89313	3.89234	
С			0.16458	0.14541	0.14522	0.09002	0.14108	0.20449	0.20460	0.22675	0.16458	0.18369	0.20000	0.22718	
F			2.57939	2.54937	2.55291	2.46410	-1.80124	-1.97527	1.97181	-2.03180	2.57939	1.84317	0.25000	1.28789	
-	Facet	2	4.13039	3.98981	3.98888	3.58353	3.42901	3.86105	3.86230	4.01328	4.13039	4.17745	4.10000	4.10701	
0			0.19632	0.17673	0.16686	0.11577	0.16625	0.22737	0.23359	0.25597	0.19632	0.21487	0.22786	0.25535	
٥	7		2.65376	2.62785	2.80928	2.62732	-1.89846	-2.16622	-1.99138	-2.04815	2.65376	1.87032	0.23013	-1.28070	
8	Facel	1	4.36645	4.22328	4.17479	3.78748	3.59706	4.00140	4.06710	4,22016	4.36645	4.40361	4.29670	4.30920	
A			Point 1	Point 2	Point 3	Polni 4	Point 5	Point 6	Point 7	Polnt 8	Point 9	Start of scan line	Middle of rotation	End of scan line	
		07 G3							,						

F14. 1383 F145. 13B3A and 1385B

MR2



Column C		Γ	I	-		1	2.12116	5	181	3	242	5		3	5	3		Ē	2659	9 19610		Ž		1
Faces Face	S	_		_		j		_		1					Ĺ	Ĺ			_	L	ļ			
Face Face	œ				:		0.6039	0.5116	31.0	200	100	1 2710		- 100	. 4705	4 8 7 8 6		900	0000			0.64.71		
Faces Face	•			Facel	-	•		,		421626	3.94486	9,000	2	1383	1 1 2024	4 2006		4.42086	441147			4.40142		
Faces Face	٩				1		2,02051	2 13458		213512	2.48515	0000	2	2.19018	2 18074	90000	8	2883	2 00027	200	,	2.00470		1
Faces Face	G	1			+		0.58809	163163		0.48704	0.21047			1 BC374	1 70944) Transition	0.56909	0000		3	A.89357		
Faces Face	2			Facel	-	n	4.59494	4 20788	3	4.39672	377405		3.7	4.30150	2000			4.59AP4	4 4780B		B (C.	5,5039	-	1
Faces Face	2	1	_		-	-	1,92423	5	A.WO.K	2.02852	2 27807	t	2.7822.5	2 04019	2000	9	199174	1,82423	30108	3	9126	1.82507		
Faces Face	ŀ	1	-	-	1		0.57105	7,000	200	0.48315	0.077.0	3	. 82124	2 17 143		3	-2.27578	0.57105	2	3	0.0000	1.19817	I	
Faces Face	ļ	1	_		3	•	4 78148		30105	4 56109	90	3	4.12497	4 4017		4.48172	4.64489	4.76148	200	9	4.74968	1,76001		
Faces Face	ŀ	•	_	İ			1 RESERT		3	1,98856	l	1	23.40	40000	5	2.01372	1,92,182	1 AAAA		1	1.89000	1870K3		
Faces Face		-		l			0 4380a		0.456	O KOOSB		200	718		20.0	2.01960	-2.11752	OGC O	}	000	00000	500		
Faces Face		-		1	Facel	-	1000	2	4.6754	464000		8	4.08721		2	4.60668	4,76563	4 85771		4.83/35	4,83795	552		
Faces Face		9					· Biney	/CD 07	1,91616	1 01057	3	2,22,561	2.20A44		X Y	194791	1.88490	. 0.007		1.62778	1.82778	1 00790	3	
Facet Face		L		1			13.00	à i	046655	20,120	7	0.20212	. PA717		2.178.22	-2.17219	227009	20.00	2	0000	00000	1 33000		
Faces Face		ш			Facel	-	9	2	4.77198	Į.		4.24022	4 26003	1	4.71924	4.72049	4 86407			4.92R26	4 97 828	10000	*,50400	
Faces Face		٥	l					1.78.14	1.86123		3	2.17873	47000		1.91714	1,88125	1 7000		2	17422	17.622	1	1.73128	
Pohi 1 Pohi 2 Pohi 3 Pohi 3 Pohi 3 Pohi 4 Pohi 5 Pohi 5 Pohi 5 Pohi 6 Pohi 7 Pohi 7 Pohi 7 Pohi 7 Pohi 8 Pohi 9 Pohi 9 Pohi 9 Pohi 10 Pohi 1		U						0.52476	A 4442B	1	3	0.28599	2000	Š	-225670	2.04739	2 17045	3	0.32478	0.0000	0000	3	-1 144 32	
		a		-	Facel		-	5.0408	4 87047		4.8173	4.20129		2	4.77372	4,62579	4 000718	,000	2000	3,02090	COUCA	3	0.0000	
						ĺ		200	Date:	2	Popula	Point 4	1	Charle	Pora	Pofrt 7	1	0110	Ž,	and of acen line	Action of someone		and or econ line.	
																				1			_	
				ø	ā		202	90			5	 -	1	2	7	,		2	3	-		اه	<u> </u>	5

FIG. 1441 FIGS. 14AIA and 14AIB



	r	_		٠,	_		_	_	_		.,				_		_	_	_	_		_	_	_
		S						00000	(1221)		3	0.18182	CACALO		0.46974	0.48974	0.646		0.000	0000	00000	3	037020	
	ľ	Œ						0.44891	0.37322	2	200	024084	1164117		1.74631	1.74831	9000	3	200	00000	2	3	47660.	
	·	0			Facel	•	1	3.52125	3.2508	3 226.00	9	2.88199	3.10607		3.47156	3.47168	7 66747		302123	3.56687	4 60CBY	3	3.67905	
			l	1	_		1	0.02	2000	0000	3	9990	95856	-	200	0.70712	0.774.0		9	0.525	0 18726		0.36428	
	ŀ	0	ľ			-		C. 440.74	0.37385	CHRYPIN	3	3	30008	2007.0	3	-2.15188	2 20000		3	0.0000	00000		1.40003	-
		2			5	47	2000	72025	3.74847	37446		27.50	220187	2000	200	3.88651	4 06330		200	3.98533	3.99543		4.05.57	
		Ξ		l			40500	200	0.100	770010	1	2	0.78 20.00 2	997100	9	0.91496	0.97183		3	0.23305/	0.25308	200.00	0.73353	
		1		f			7777	Š	0.37427	0.37427	A AMPLE	COTTO	-2.41913	2 KOORK		2.52933	2.57881	17077		0000	00000	2	3	
	*	4		ŀ	180	•	4 20.776		4.14124	4.14124	0 709ED	3	3.69153	4 24507		423097	4.4114			1000	200	773.65	3	_
	-	•		f	1	_	0.777.0		200	20.0	70000	3	0.74455	80000		9000	0.06529	017770		2000	00000	0.74880	7	
	_			l	†	_	03777		ž.	0.48536	0 20147		.2.24BO/	2 4500		7/77	÷2.38443	957		2	00000	1 53417		
	1			Faces	8		4 49170	I		1,28311	270		73/76	4.3743		-	1,37811	4.49170		3	2000	462189		_
ļ	9				1		0.22157	7700		0.19826	0.13371	20000		222	VALUE OF	2000	3	0.22157	0.346.0		200	0.82947		
		ĺ		ľ	t		0.44811	A4777.0	200	0.37701	0.15472	2 22 6		2,46863	2 ACADO	3	5	97	0	3 3	333	-1.65515	l	
ļ	_	İ		FRCA	•	۲	6550	5	3	4 30022	4.04852	4 17480		4.59519	4 40027		1	63300	A READS		3	602		
	-	İ			İ		026978	0.24452		0.16/40	0.15299	O BAOOS		.02367	7,000		3	0.26970	O 3HBDA	2000	2	96629	-	1
ļ	۔						0.44237	C369C 0		0.7401	0.22763	2 24 500		Ç.	2.30530	2000	3	653	00000	2		.1.51167	ŀ	1
		l		Fecel	-		8	4.86874	4 000	61,700	4, 18842	4 29178		4.03 107	4.74716	1 804.13		8	4.82442	4 83443		1.04.361		
		ľ				1	Louis	Point 2	Police 3	2	Politi	Point	1		Pohi 7	Dodos		5	and of scan fine	Aindle of rotation		EDG OF SCHOOL		
•							i										ĺ	-	Series	Minda		5		
					8																			
	1	2	ĺ	ğ	107	1	3	8	3	İ		7	Ė	1	Ĭ	1	ŀ	j	-	118	ŀ		8	

FIG. 14BL FIGS. 14BIA and 14BIB





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٢	Γ	, ,		ĝ	2	3	974	1874	0.56463	8	085	9	Š	ı
S				ľ	Ľ			Ĺ	Ĺ	Ş	0.0438	L	100	
_		0.44	0 1770	0.37322	024084	-1.84117	1,74831	-1 74831	1.61036	0.44891	0,0000	0.0000	1.09574	
0	Facet	9	2017 C	332508	2,86188	3,10607	3.47166	3.47166	3.68342	3.52125	3,56887	3.56887	3,67,805	I
•		o control	2007	00000	0.10588	0.50656	0.70794	0.70712	0.77533	0.02505	0.15325	0.152251	0.36428	
0		70077	23,384	0.37600	0.15541	-2.00085	-2.15830	-2.15188	-2.20429	0.44834	000000	00000	1.40030	
z	Facet	C COOK	3.74847	3.74516	3.17535	329187	3.86517	3,89631	4.08339	3.93952	3.96552	3 96553	4.08537	
2		A 19160	1001	0.10044	0.04285	0.78626	0.91486	0.91468	0.97183	0.12563	0.25305	0.25305	0.75509	
- -		77077	0.374.27	0.37427	0.20355	-2,41913	252855	2.52955	-2.57881	0.44954	0.0000	0,00000	1.71403	
¥	Facel	1	1	4.14124			1	l		Ĺ	4,32801	4.32801	4.47185	
ſ		- Marie 0	0.15017	20.10	0.05234	0.74455	0.92829	0.90666	62586.0	0.17770	0.30000	0.30000	0.74880	-
_			0.37132	П	i		[]		2.38443			1	53817	
Н	Facel	<u>:</u>	4.31949	Ш	3.79612						90000	L	62168	
×	1	1		П						1	1	٦	Ī	L
0			1	0.18626				١,		0.22157	0.34528	0.34526	0.82987	
		0.44811	0.37345	10770.0	0.15472	-2.32513	-2.46963	-2.46486	-2.51341	0.44811	0.00000	0.0000	-1.85515	
3	Fecal	488.02	4,50100	4.50022	4.04652	4,17480	4.59519	4.59627	4.74099	4.65500	4.66490	4.66490	4.60210	
٥		0.28976	024652	0.18746	0.15299	0.84826	1.02367	0.99034	1,04372	0.26978	0.38908	0.38807	0.82998	
٥	-	0.44237	0.36963	0.54811	0.22763	2.24588	-2.48257	-2.30530	-2.35178	0.44237	0.0000	0.0000	1.51167	_
a	Facer	185/80	4,66874	6,62719	4,18842	4.29178	4,69167	4.74716	0.89443	4.82498	4.82442	4.62442	4,94381	_
		Point	Point 2	Poht3	Point 4	Point 5	Point 6	Point 7	Point 8	Polnt 9	Start of scan line	Middle of rotation	End of scen line	
	80	3	601	110	Ξ	12	2	2	5	9	1	<u> </u>	2	8

FIGHTHEL FIGS. 14CIA and 14CIB

<u>:</u>





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S	L			ğ	Q	φ.1.	9.5	8	ő	9470	Ϊ	Ď,	Š	0.0436	S	٤	3	
æ				Į	0.37322	0.37322	0.24084	-1.84117	174831	1 74831	1	1	0.44891	0.0000	00000	4 CACA 74	COY I	
0	Facel	•	٩	3.52125	3.32508	3.32508	2.99199	3.10607	3.47188	3.47186		385	3,52125	3.56687	3,56887	2000	0.00/0.0	
a.				0.02505	-0.00784	-0.00933	0.10566	0,50856	P5/070	0 201213	2	0.77533	0.02505	0.15325	0.15325	200	0.30	
0				0.44834	0.37385	0.37803	0.15541	2,00085	0.351 6	00131	8 13	2.20428	0.44834	0.00000	00000	ļ		
z	ğ		•	3.93952	3.74647	3.74518	317535	3.29187	7 04517	2 640 6	2000	4.06039	3.93952	3,96553	3.05953		1780	
2	İ			0,12583	0.10044	0.10044	0.04285	O 7RR76	0.01458	3	9	0.97183	0.12583	023305	20200		0.75309	
	İ			0.44954	0.37427	0.37427	0.20185	-241917	2 6 3 0 6	2000	Š	-2.57691	0.44954	00000	0		1.71403	1
¥	1	3	7	4.30775	4 14124	4 14124	3 76350	180107	10030	10000	123.53	4.114	4.30775	4.32901	.000	1	Ì	
,				0.17770	21051.0	0	2000	24486	3	1			ŀ	1		1	0.74680	
-				044459	0.171.0	20,437.0	20.72	2000	2	7 300	.2.3374.3	-2.38443	0.44459	10000	10000	3	-1.53817	
Į		ē	<u></u>	4 40179	73.60	4 26011	0.000	3,000	3,000	7	4.1130	4.57811	4.49179	1 40000		3	4.62188	
c	,			0 22147	700	0.000		0.1357	3	0,39272	0.9920	1.04484	022157	D TAKE		C. Y.	0.62967	
-				0.44811	37.54	i	ı	T	ł	1	-2.4648 <u>6</u>	2.51341	Ī	Τ	ľ	O.MOO	-1.05515	
u	ŀ	1808	2	A RKKINS	L	1	1	3		BICKE		L	L	l	200	9.00	4.80210	
ļ]			940000	2000	715	1	֓֟֟֟֟֟֟֟ <u>֚</u>	CONSCE	1.02567	0.88034	10432	A 2607A	00000	11.303.00	0.3650	0.62996	
ļ	·			44222	0 0000	2	1000	3/27	-2.24568	2.49257	230630	275176	11077	2000	3	88	-1.51167	
		TO S		007700		Î	4.62718	4 10042	٦	4,69167	4.74718	A BOARS	١		7	4.04.4	4.94361	
	*			Peter	- India	ZILOL	Form 3	Point 4	Poet	Point 6	Potra 7	Doing 8	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	A LEON	SIZIN OF SCEN FINE	Middle of rotation	End of actan line	
۱			100	3								1	1					

F1G. 14D1 Plys. 14131 A and 14D1B



s			9.26544	5.40895	5,40695	5.65479	523668	4.98858	4.98859	4.84810	52854	521121	521120	4.84743	7
ч	_		0.34512	0.28706	0.28708	0.18544	3.08048	3,12802	3,12902	3,16638	0.34512	0.00006	0.00000	-2.50435	
0	Fecel	9	8.87159	6.81701	6,81701	6.72143	6.22148	6.28421	628421	6.32024	6.87159	0.82144	6.82143	8.44831	
_			4,74102	4.88659	4.69784	5,31804	4,82441	4.49196	4.49112	4.34377	4.74102	4,69680	4.59679	4,35990	
0			0.35881	0.30018	0.30354	0.12498	-2.80040	-2.92071	-2.91718	2.85743	0.33981	0.00007	0.0000	.2.26763	
z	Fecet	0	7.03508	6.97894	6.97521	6.81288	6.36745	8.47684	6,47758	6,51493	7.03508	8.97902	6,97801	6.84346	
Σ			4.28573	4,39726	4.30726	4,66313	123771	3.86682	3.96692	3.84879	4.26573	4.22381	4.22382	3.85384	
7			0.35054	0.29192	0.29182	0.15884	-2.93734	-3.02659	-3.02659	3.08018	0.33054	-0.00002	000000	-2.39464	
¥	Facet	•	7.17887	7,13030	7.13030	7.02005	6.55131	6.61899	6.61699	6,64613	7.17887	7,12380	7.12389	6.77390	
•			4.03445	4.16842	4.19794	4.57132	4.17809	3,80174	3.78090	3.64875	4.03445	100001	4.00000	3.66997	
-			0.36293	0.30320	0.39665	0.16475	2.72089	-2.69597	-2,79811	-2.83603	0.38283	0.0000	0.0000	-2.14504	~
•	Facel	6	725212	7,20014	7.20860	7,04932	6.61109	8.69286	6.71616	6.75093	7.25212	7.19246	7.19245	6.87835	
9	1		3,81836	3.93288	3.93374	4.26827	3.83654	3,51184	3,51128	3.40022	3.61938	3.78342	3,78335	3,41071	
			0.35437	0.29548	0.29830	0.12287	l	L	L	2.89436	ı	1	ı	-2.31840	
ш	E G	2	7.31676	-	ľ	ı		L	L	8.79682	ı	ŀ	Ĺ	ļ	
-			3.80007	3.77280	3.76848	4,09695	3.68330	3,36219	3,32225	321407	3.60327	3.37345	3,57301	323472	
٢	,		12990	0.30577	0.45214	0.19069	-2.71194	-2.91744	2.78529	-2 BO469	129950	0,00361	00000	2.11473	
ď	2	-	7 39483	233669	7.35085	7 19969	8.76168	ſ	1	Γ	7,38483	7.32281	1,30205	7.01771	
_			Doing 1	Polnt 2	F and	Point 4	Point 5	Point 6	Point 7	Point 8	Point	Start of scen line	Middle of contino	End of scentine	
	946	i di	3	502	120	111	-12	111	1	-	1.0	1	118	100	83

F14. 1543 F1GS. 15A3A BUNCL 15A3B

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PIGS.	
F14-1583	



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•	_	_	_		_	3	F	-			1						,		
		ļ	-		ŀ		Facel		_	_	Face Sec			Š		1	8	Ì	١
-	100	1			t		•		ļ	-	-		L	40			9		
	-		-	~	1	1	7	I				4.9	V 04000	80500	135081	4 74102	6.87159	0.34512	526544
Dodne 1	L		60027	7.31635	0.35437	3.91836	7.25212	1	٦	1	1	1	Į	ı		02000	102.10	A 28778	4000
			500	97070	0.20448	191289	7 20014	ŀ	•	7.13000				١	200	2	200		
2 100		i	207				20000	l	ľ	ı	ı				30354	4,88764	6.61701	028708	9
Potra 3 7.3	7.35085 0.4		76848	727048	0290	3,83374	740000	1	1	ł	١	ľ	١		12490	5.31804	8.72143	0.18544	5.65470
ļ			56960	7,13404	0,12287	4.26827	7.04932	١	1	1	١		ĺ	ľ	POO 40	1 400441	8.2214B	3.06048	\$23666
Point S. 8.7	0.76168 -2.7	ı	06668	6.60269	2,84072	3.83654	9.01109	1	ľ	i	1	Ţ	ı	Т	0000	001077	6.20421	912900	4.96858
ľ	8 82335 -2.8		36219	6,76969	2.95787	3.51184	6.63286	1	1	١	١	1	l	1	01000	211077	8 28471	212000	4 9885B
Γ	L	ı	33225	6.77043	2.05483	3.51128	6.71818		"	Ì	1	1	١	1	0.000	1	1000	STAN C	4.84610
	L	l	21407	6.79682	-2.99438	3.40022	6.75093		1	ł	1			0.51465	20000	20,74	8 97140	0.34512	3.28544
	L	0,36621	3.60327	7.31635	0.35437	3,61936	7.25212	0.36290	4,00443	7.17887	1	0.35054	7.5057.3	١	0.0000	100000	777.00	00000	321121
ľ		19000	57.75	7.25900	950000	3.76342	7,18248		Ì		Ì	1	1	19/8K	,				200
ľ	1	١		2410	į	2 707.76	7 10045	ı	ľ	7.12389	_	20000		1964	00000	4.000	7	3	
Aiddle of rotation 7.3	00		100	7000	3	3		ı	ľ	ľ	ľ	ļ	ľ	RATAR.	2 267 63	4.35980	253	3	7
End of scan line 7.0	.01771] -2.1	£3	23472	B. 82439	2.31840	141071	6.67833	Ž.		1	1		L		-	-			
			_	_						-			1		1				

F14.15C3 F1GS. 15C3 A and 15C3B



S			26544	40895	40895	85478	323606	96656	9883	94610	28.4 28.4	21121	21120	
	L	L	12	80	90		ľ	ľ	•	8	٦	Ľ	9	
Œ			0.34512	Ī	i					-3.16839	ı	0.00008		
0	Facet	8	6.87159	8,81701	6.81701	6.72143	6.22148	6.28421	6.28421	6.32024	6.87159	8.62144	6.62143	
.			4.74102	4.88659	4.88784	6.31804	4.82441	4.49196	4,48112	4.34377	4,74102	4.69690	4.89879	
•			0.35961	0.30018	0.30354	0.12498	2.80040	-2.92071	2,91719	2.95743	0.35981	0.00007	0.0000	
z	Facet	S	7,00500	6.97894	6.97821	6.61286	6.36745	6.47664	8,47758	6.51493	7,03508	6.97902	6.97901	
1			4.26573	4.38728	4.38726	4.66313	4.23771	3.99682	3,98632	3.84679	4.28573	4.22381	4.22362	
-	L		0.35054	0.29192	0.29182	0.15884	-2.83734	-3.02659	3,02659	-3.08618	0.33054	0.00002	0.0000	100000
×	Facet	.,7	7.17887)	7,13030	7,13030	7.02005	6.56131	6.61699	6.61699	8.84813	7,17867	7.12389	7.12389	-
	H		4.03445	4.18642	4.19784	4.67132	4.17939	3.80174	3,78090	3.64875	4,03445	4,00001	4.00000	
	H		0.36293	0.30320	0,39685	0.18475	2.72069	2.88597	2,78611	2.83800	0.36292	0.00004	0.0000	
ı	Facet	3	7.25212	7.20014						6.75093				20000
0	L		909183		3.93074	L				3.40022		3.78342	ĺ,	
	L	L	35437 3	L		Ì		2.85787 3				3,000.0		Loresco
1	1908	2	Ĭ	8					Ĭ			ľ		
9	Œ		7.31635	7.2701					Ī	0.79662			7.25882	ľ
٥			3.60327	3.72280	3.7684B	•	r		ď	321407	3,60327	3.57345	3.87301	
ပ			12986.0	0.30677	0.45214	0.19089	-2.71194	-2.91744	2.78529	2.60469	0.36521	0.00361	0.0000	65716
8	Facet	-	7,38483	7.33669	7.35085	7 19969	6.76168	6.62333	6.66198	6.69054	7,38483	7.32381	7.32.325	1000
		-	Point 1	Point 2	Poim3	Pom 4	Point 6	Point	Point 7	Potm 8	Pohn 9	Start of scen line	Middle of rotation	and of the last
<														
Н	8	07/03	8	8	ē	11	12	판	1	S.	16	17	2	a

14. 1503 RGS. 1503A and 1503B